



RELIABILITY OF CORRODED STIFFENED PLATE SUBJECTED TO UNIAXIAL COMPRESSIVE LOADING

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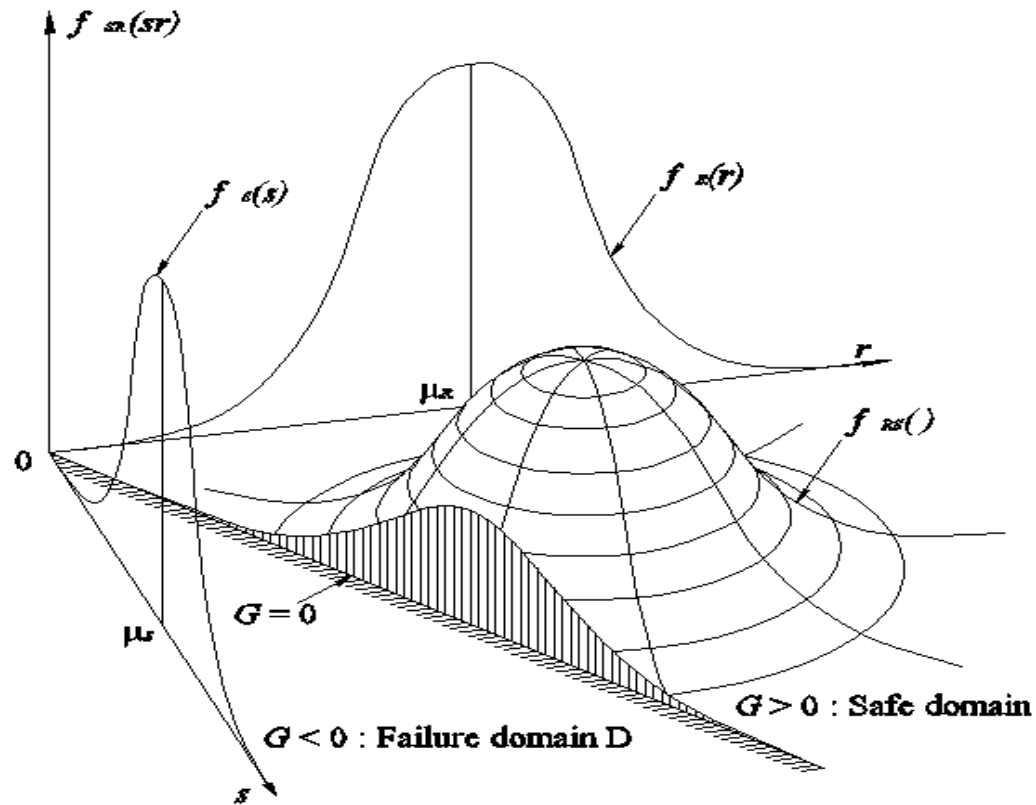


Objectives

- **Investigation of the reliability of corroded stiffened plates subjected to compressive uniaxial load**
- **Comparison between two corrosion models**
- **Consideration of uncertainties related to mechanical properties, thickness and level of initial imperfections**
- **Discussion about the origin of the uncertainties and their impact into the reliability**



Basic structural reliability definitions

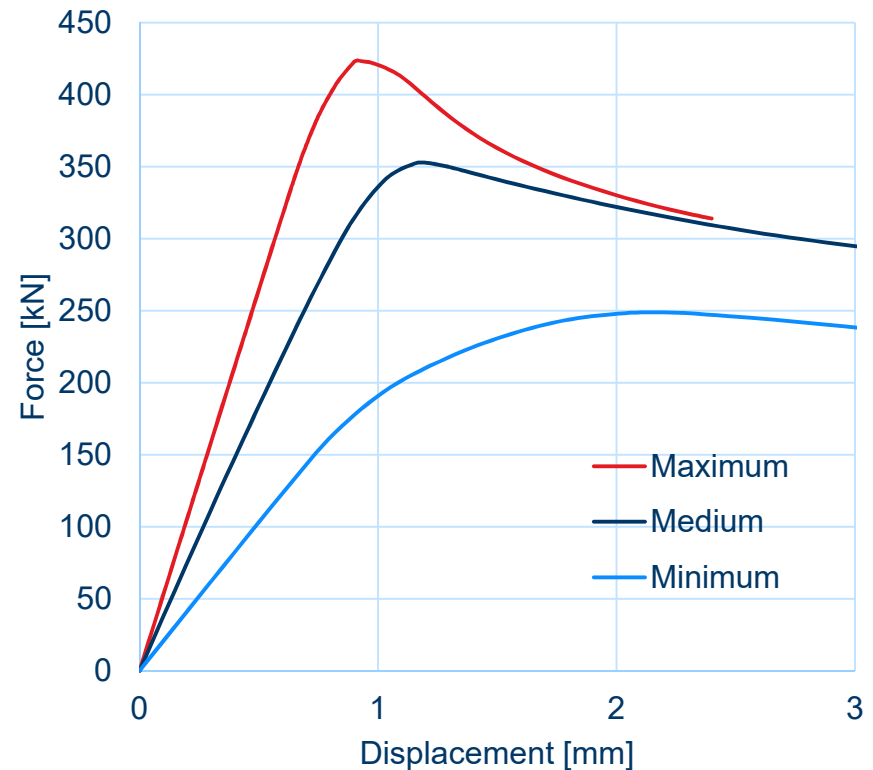


Source: Melchers, R. E. 1999. *Structural reliability: analysis and prediction*, Chichester, John Wiley.



Ultimate strength – basic informations

- **Ultimate strength depends from many factors, including initial distortions, mechanical properties, corrosion degradation and presence cracks.**
- **The ultimate capacity is subjected to high uncertainties with respect to stochastic variations of considered factors**
- **Recent studies revealed that not only thickness is reduced with corrosion development, but mechanical properties too**



Source: Woloszyk, K., & Garbatov, Y. (2019, August). Uncertainty assessment of ultimate strength of corroded stiffened plates subjected to maintenance. In *Sustainable Development and Innovations in Marine Technologies: Proceedings of the 18th International Congress of the Maritime Association of the Mediterranean (IMAM 2019), September 9-11, 2019, Varna, Bulgaria* (p. 429). CRC Press.



Stiffened plate failure modes – according to Common Structural Rules

- **Beam column buckling**

$$\sigma_{CR1} = \begin{cases} \sigma_{E1}; & \sigma_{E1} \leq \frac{Re}{2} \\ Re \left(1 - \frac{Re}{4 \sigma_{E1}} \right); & \sigma_{E1} > \frac{Re}{2} \end{cases}$$

- **Torsional buckling**

$$\sigma_{CR2} = \begin{cases} \sigma_{E2}; & \sigma_{E2} \leq \frac{Re}{2} \\ Re \left(1 - \frac{Re}{4 \sigma_{E2}} \right); & \sigma_{E2} > \frac{Re}{2} \end{cases}$$

- **Web local buckling**

$$\sigma_{CR3} = \begin{cases} \sigma_{E3}; & \sigma_{E3} \leq \frac{Re}{2} \\ Re \left(1 - \frac{Re}{4 \sigma_{E3}} \right); & \sigma_{E3} > \frac{Re}{2} \end{cases}$$

Source: IACS 2015. Common structural rules for bulk carriers and oil tankers. London: International Association of Classification Societies..



Limit state function

$$g = \widetilde{X}_R \widetilde{X}_I \widetilde{\sigma}_U - \widetilde{\sigma}_L$$

\widetilde{X}_R - uncertainty parameter related to welding-induced stresses (normal random variable with mean value of 0.95 and standard deviation of 0.05)

\widetilde{X}_I - uncertainty parameter related to initial imperfections (normal random variable with mean value of 1.00 and standard deviation of 0.05)

$\widetilde{\sigma}_U$ - random variable of ultimate stress, minimum from three failure modes:

$$\widetilde{\sigma}_U = f(\tilde{t}, \widetilde{Re}, \tilde{E})$$

$\widetilde{\sigma}_L$ - loading (normal random variable with CoV=0.1)

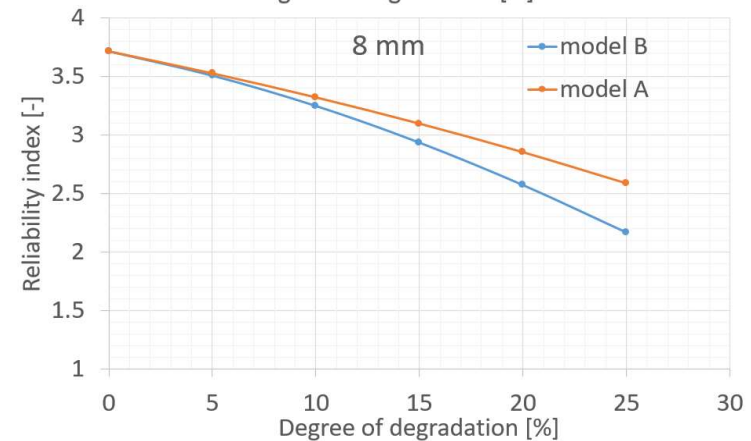
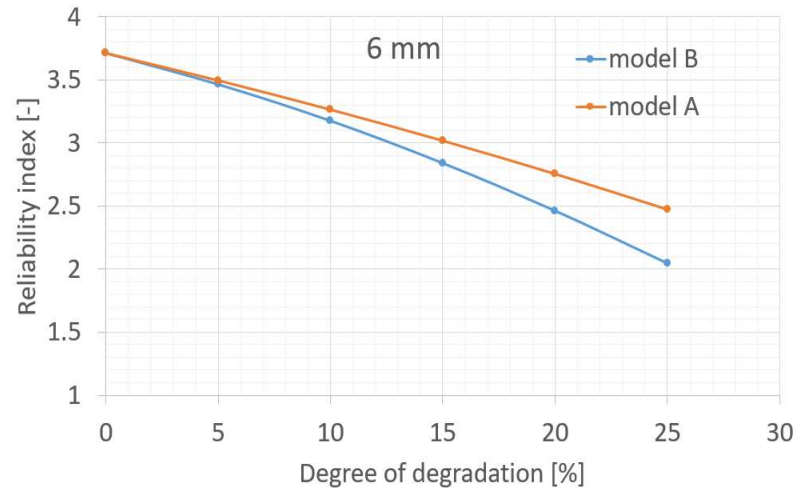
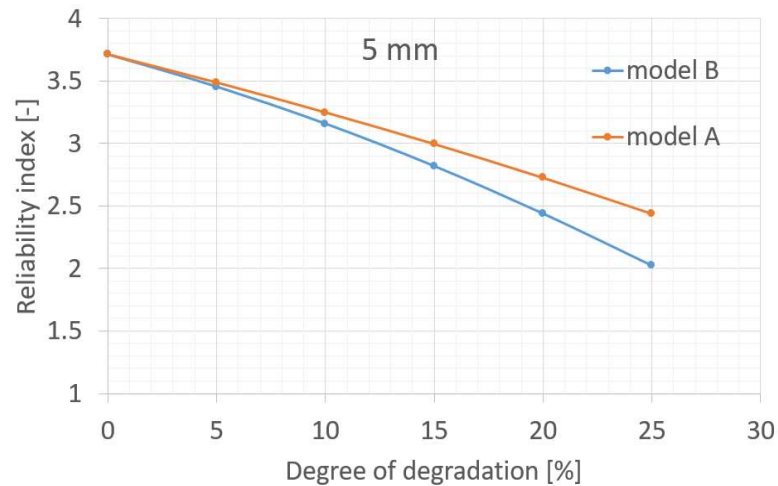


Random variables descriptors

| DoD [%] | Thickness t [mm] | | Yield Stress Re [MPa] | | Young modulus E [MPa] | |
|-------------------|------------------|----------|-----------------------|----------|-----------------------|----------|
| | Mean value | St. dev. | Mean value | St. dev. | Mean value | St. dev. |
| 5 mm plate | | | | | | |
| 0 | 5 | 0.0685 | 235.0 | 7.11 | 196.0 | 23.1 |
| 10 | 4.5 | 0.0771 | 238.3 | 7.11 | 185.7 | 23.1 |
| 25 | 3.75 | 0.0897 | 234.6 | 7.11 | 170.1 | 23.1 |
| 6 mm plate | | | | | | |
| 0 | 6 | 0.0822 | 235.0 | 7.11 | 196.0 | 23.1 |
| 10 | 5.4 | 0.0925 | 238.3 | 7.11 | 185.7 | 23.1 |
| 25 | 4.5 | 0.1077 | 234.6 | 7.11 | 170.1 | 23.1 |
| 8 mm plate | | | | | | |
| 0 | 8 | 0.1096 | 235.0 | 7.11 | 196.0 | 23.1 |
| 10 | 7.2 | 0.1233 | 238.3 | 7.11 | 185.7 | 23.1 |
| 25 | 6 | 0.1435 | 234.6 | 7.11 | 170.1 | 23.1 |



Results



Model A – only thickness reduction is considered

Model B – both thickness, and mechanical properties reduction are considered



Impact of corrosion measurement data

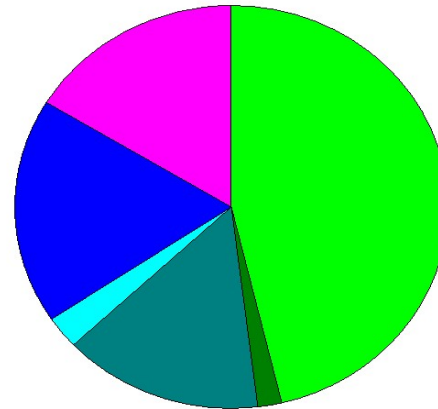
| DoD [%] | Initial thickness [mm] | Corrosion depth [mm] | |
|---------|------------------------|----------------------|--------------------|
| | | Mean value | Standard deviation |
| 0 | 5 | 0 | 0.19 |
| 10 | 5 | 0.5 | 0.28 |
| 25 | 5 | 1.25 | 0.40 |
| 0 | 6 | 0 | 0.19 |
| 10 | 6 | 0.6 | 0.30 |
| 25 | 6 | 1.5 | 0.45 |
| 0 | 8 | 0 | 0.19 |
| 10 | 8 | 0.8 | 0.33 |
| 25 | 8 | 2.0 | 0.53 |

| DoD [%] | Initial thickness [mm] | Reliability index [-] | | Difference [%] |
|---------|------------------------|-----------------------|-----------|----------------|
| | | Exp. | Real data | |
| 0 | 5 | 3.71 | 3.72 | 0.2 |
| 10 | 5 | 3.16 | 3.09 | 2.0 |
| 25 | 5 | 2.02 | 1.88 | 6.9 |
| 0 | 6 | 3.71 | 3.72 | 0.2 |
| 10 | 6 | 3.17 | 3.14 | 1.2 |
| 25 | 6 | 2.04 | 1.92 | 6.0 |
| 0 | 8 | 3.71 | 3.72 | 0.2 |
| 10 | 8 | 3.24 | 3.23 | 0.3 |
| 25 | 8 | 2.16 | 2.07 | 4.2 |



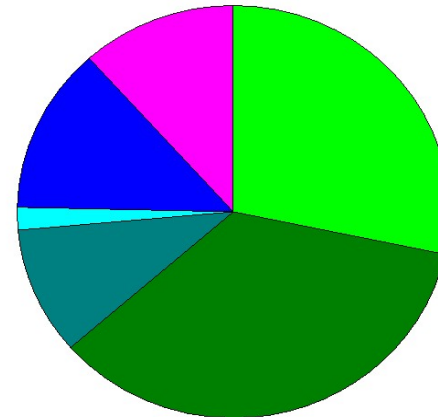
Sensitivity factors of reliability analysis

Uncertainty of thickness based
on experiment



| | |
|----------------------------|-------|
| in | 0.40 |
| re | 0.43 |
| Re | 0.16 |
| E | 0.39 |
| t | 0.13 |
| Lo | -0.68 |
| Sum of a ² 1.00 | |

Uncertainty of thickness based
on in situ measurements

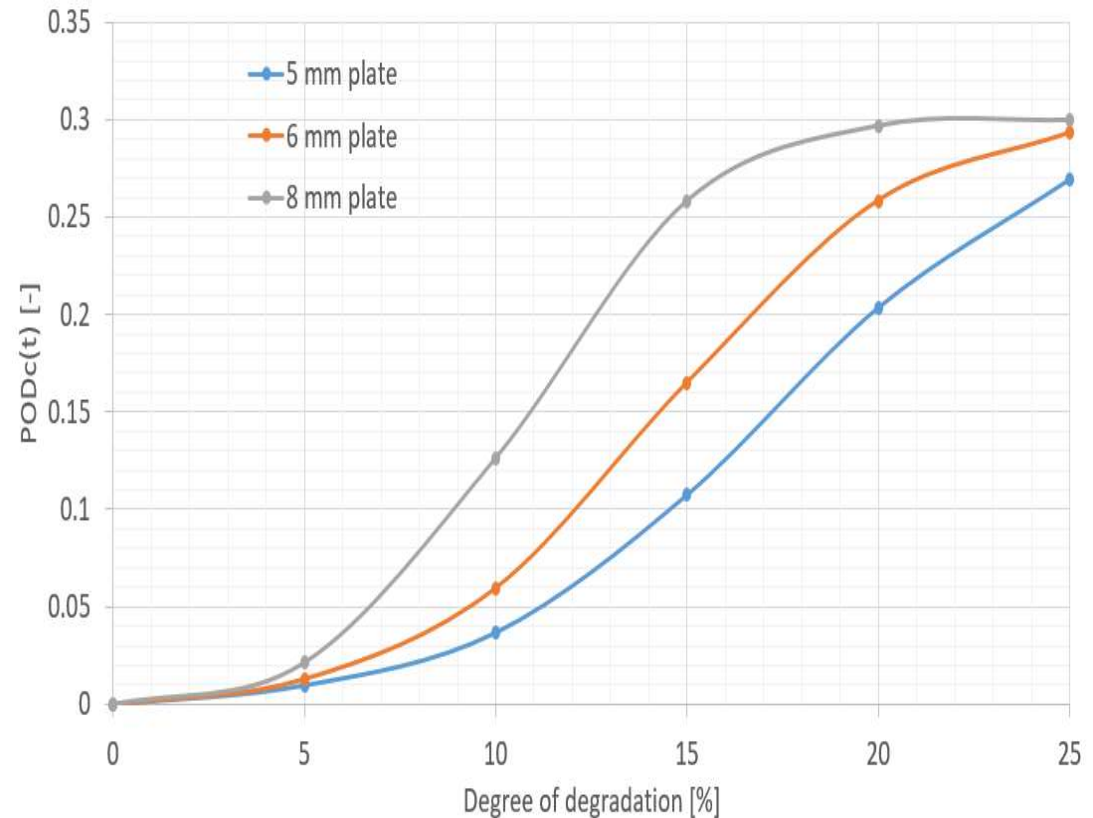


| | |
|----------------------------|-------|
| in | 0.34 |
| re | 0.36 |
| Re | 0.14 |
| E | 0.32 |
| Lo | -0.59 |
| d | -0.53 |
| Sum of a ² 1.00 | |



Probability of detection

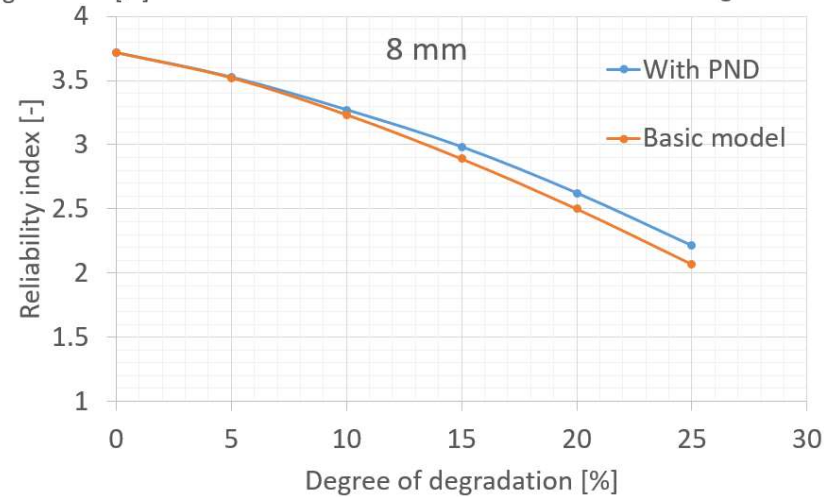
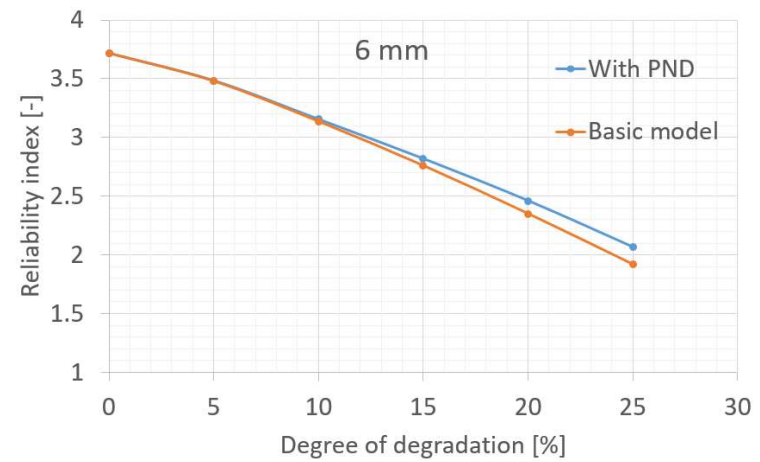
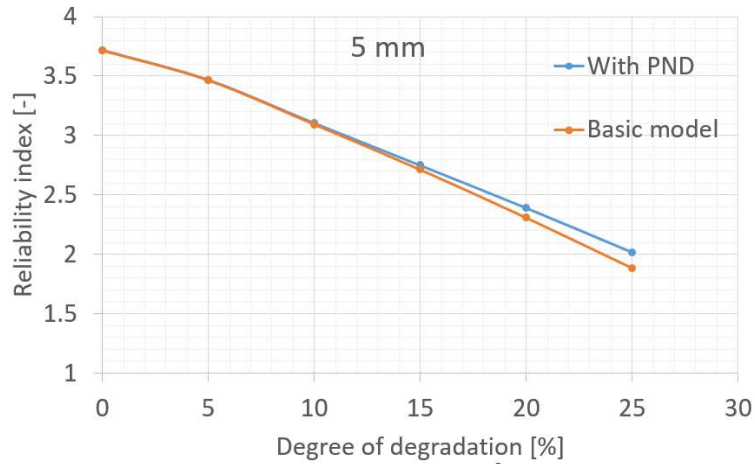
- Only structural component omitted during inspection may fail
- Reliability formulation is extended considering probability of non-detection
- More severer corrosion is easier to be captured compared to moderate one



Probability of detection for considered plates



Impact of detection probability





Conclusions

- **A simplified approach to assess the reliability of corroded stiffened plates was presented**
- **The presetend approach is fast and practical, with comparison to e.g. advanced nonlinear FE analysis with multiple random runs**
- **The reliability index is significantly lower, when both thickness and mechanical properties reduction are taken into account**
- **The reliability formulation is very sensitive with respect to origin of uncertainty formulations**
- **Further studies related to uncertainty quantification are essential**
- **The reliability index is slightly higher, when only structural members with nondetected severe corrosion degradation are considered**



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